

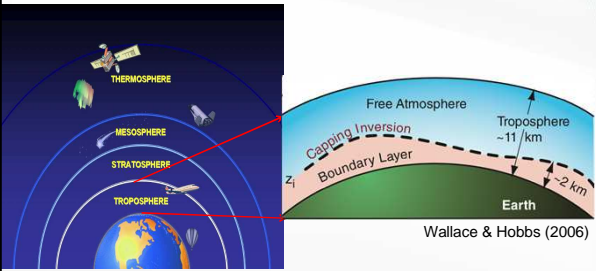
大气边界层流体运动的湍流机制方程及其结构的相似性理论描述






周新华
Campbell Scientific, US
第14次 ChinaFLUX 通量理论与技术培训
2019年8月6日

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Wallace & Hobbs (2006)



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边界层流体：
以水平流动为主的含水热的空气湍体




湍流的成因

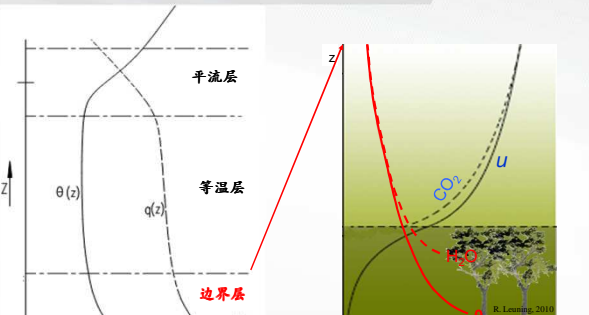
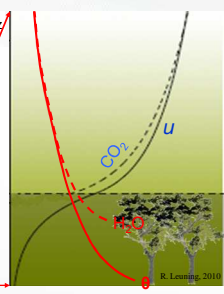

1. 与下垫面摩擦引发的水平风速随高度而变的梯度
2. 与下垫面热交换，空气密度改变所产生的空气浮力

内部特征

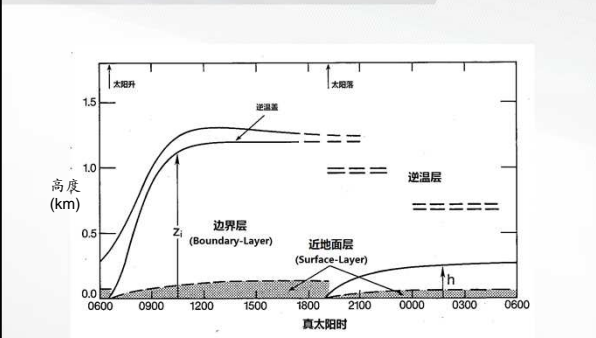
1. 三维无规则运动
2. 各气体组分不断地混合




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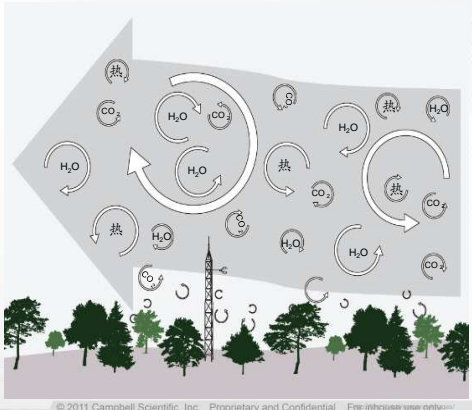


对流层：随太阳升起对地面加热而抬升活跃，随太阳降落与地面冷却而降低变稳 (Kaimal & Finnigan 1994)



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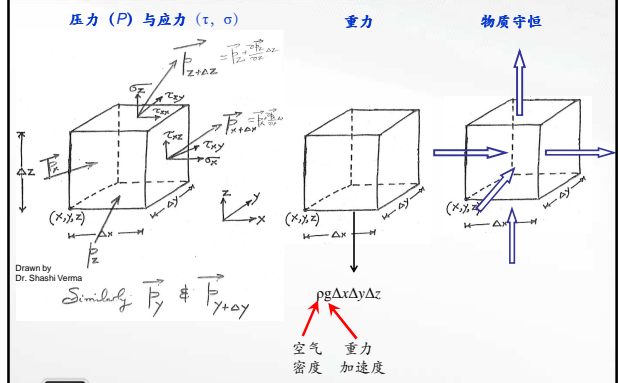
湍流传输CO₂/H₂O/痕量气体



以上的六张图片

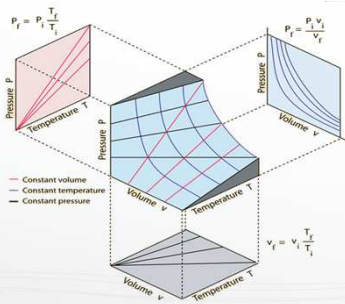
1. 边界层及其高度
2. 湍流的产生和耗散与其随机运动
3. CO₂/H₂O/温度/风速垂直梯度 (结构)
4. 湍流传输CO₂/H₂O/热

流体运动的物理数学描述



状态方程 (Equation of State)

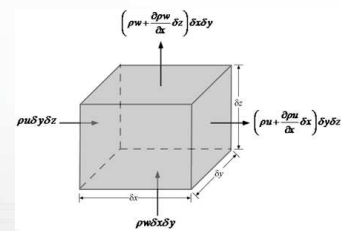
$$P = \rho RT$$



连续方程

Continuity Equation

$$\frac{\partial \rho}{\partial t} + \rho \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) = 0$$



描述流体的基本方程

状态方程 $P = \rho RT$


连续方程 $\frac{\partial \rho}{\partial t} + \rho \frac{\partial u_j}{\partial x_j} = 0$

运动方程 $\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + \frac{\mu}{\rho} \frac{\partial^2 u_i}{\partial x_j \partial x_j} - g \delta_{3i}$

空气粘滞系数

Kronecker Delta

$x + y = 2$
 $x = 1$
 \downarrow
 $1 + y = 2$



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宝恩内恩克近似
(Boussinesq Approximation)


假设

1. 空气粘滞系数不变 ($\mu = \text{constant}$)
2. 空气为不可压气体
3. 瞬时值与参考值相对较小

	压力	温度	空气密度
参考值	P_0	T_0	ρ_0
瞬时值	P	T	ρ

$P_i = P - P_0$ $T_i = T - T_0$ $\rho_i = \rho - \rho_0$

$\left| \frac{P_i}{P_0} \right| \ll 1$ $\left| \frac{T_i}{T_0} \right| \ll 1$ $\left| \frac{\rho_i}{\rho_0} \right| \ll 1$



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状态方程的近似

$P = \rho RT$

$\ln P = \ln \rho + \ln R + \ln T$


$\frac{dP}{P} = \frac{d\rho}{\rho} + \frac{dT}{T}$

$\frac{dP}{P} = \frac{P - P_0}{P_0 + P_1} = \frac{P_1}{P_0 + P_1} \approx \frac{P_1}{P_0}$

$\frac{d\rho}{\rho} \approx \frac{\rho_1}{\rho_0}$ $\frac{dT}{T} \approx \frac{T_1}{T_0}$

$\frac{P_1}{P_0} = \frac{\rho_1}{\rho_0} + \frac{T_1}{T_0}$

$\frac{\rho_1}{\rho_0} = -\frac{T_1}{T_0}$




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连续方程的近似

$\frac{\partial \rho}{\partial t} + \rho \frac{\partial u_j}{\partial x_j} = 0$

$\frac{\partial \rho}{\partial t} = 0$


$\frac{\partial u_j}{\partial x_j} = 0$



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运动方程的近似

$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + \frac{\mu}{\rho} \frac{\partial^2 u_i}{\partial x_j \partial x_j} - g \delta_{3i}$




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净压方程

$P(z) = \int_z^\infty g \rho(h) dh$

$\frac{\partial P_0}{\partial z} = -\rho_0 g$

$\frac{\partial P_0}{\rho_0 \partial x_3} = -g$



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运动方程的近似

$$-\frac{1}{\rho} \frac{\partial P}{\partial x_i} = -\frac{1}{\rho_0 + \rho_1} \frac{\partial (\rho_0 + \rho_1)}{\partial x_i} = -\frac{1}{\rho_0} \left(1 - \frac{\rho_1}{\rho_0}\right) \left(\frac{\partial \rho_0}{\partial x_i} + \frac{\partial \rho_1}{\partial x_i}\right)$$

$$\frac{\partial \rho_0}{\rho_0 \partial x_3} = -g = -\frac{\partial \rho_0}{\rho_0 \partial x_i} - \frac{1}{\rho_0} \frac{\partial \rho_1}{\partial x_i} + \frac{\rho_1}{\rho_0} \frac{\partial \rho_0}{\rho_0 \partial x_i} + \frac{\rho_1}{\rho_0^2} \frac{\partial \rho_1}{\partial x_i}$$

$$\frac{\rho_1}{\rho_0} = -\frac{T_1}{T_0} = g \delta_{3i} - \frac{1}{\rho_0} \frac{\partial \rho_1}{\partial x_i} - \frac{\rho_1}{\rho_0} g \delta_{3i} = 0$$

$$-\frac{1}{\rho} \frac{\partial P}{\partial x_i} - g \delta_{3i} = -\frac{1}{\rho_0} \frac{\partial P_1}{\partial x_i} + \frac{T_1}{T_0} g \delta_{3i}$$



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运动方程的近似

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} - g \delta_{3i} + \frac{\mu}{\rho} \frac{\partial^2 u_i}{\partial x_j \partial x_j}$$

$$-\frac{1}{\rho} \frac{\partial P}{\partial x_i} - g \delta_{3i} = -\frac{1}{\rho_0} \frac{\partial P_1}{\partial x_i} + \frac{T_1}{T_0} g \delta_{3i}$$

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{\partial P_1}{\rho_0 \partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_j \partial x_j} + \frac{T_1}{T_0} g \delta_{3i}$$

温度波动与重力偶联
可有效地绕动气流



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热传输方程

$$\frac{\partial T}{\partial t} + u_j \frac{\partial T}{\partial x_j} = \frac{k_1}{\rho_0 C_p} \frac{\partial^2 T}{\partial x_j \partial x_j}$$

分子运动方程

$$\frac{\partial s}{\partial t} + u_j \frac{\partial s}{\partial x_j} = D_s \frac{\partial^2 s}{\partial x_j \partial x_j}$$



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运动方程

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{\partial P_1}{\rho_0 \partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_j \partial x_j} + \frac{T_1}{T_0} g \delta_{3i}$$

热传输方程

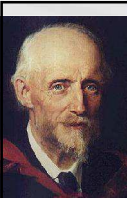
$$\frac{\partial T_1}{\partial t} + u_j \frac{\partial T_1}{\partial x_j} = \frac{k_1}{\rho_0 C_p} \frac{\partial^2 T_1}{\partial x_j \partial x_j}$$

分子运动方程

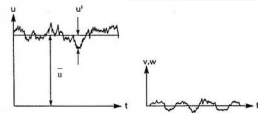
$$\frac{\partial s}{\partial t} + u_j \frac{\partial s}{\partial x_j} = D_s \frac{\partial^2 s}{\partial x_j \partial x_j}$$



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雷诺(Reynolds) 变量分解与平均规则



分解规则 $u_i = \bar{u}_i + u'_i$ $\overline{\bar{u}_i + u'_i} = \bar{u}_i + \overline{u'_i} = \bar{u}_i$

平均规则 $\bar{u} = \frac{1}{n} \sum_{i=1}^n u_i$ $\frac{\partial \bar{u}}{\partial x} = \frac{\partial \bar{u}}{\partial x}$

$$\bar{u'} = \frac{1}{n} \sum_{i=1}^n u'_i = \frac{1}{n} \sum_{i=1}^n u_i - \frac{1}{n} \sum_{i=1}^n \bar{u} = 0$$

$$\overline{u w} = \overline{(\bar{u} + u')(\bar{w} + w')} = \bar{u} \bar{w} + \overline{u' w'}$$



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运动方程描述湍流

宝恩内思克近似运动方程

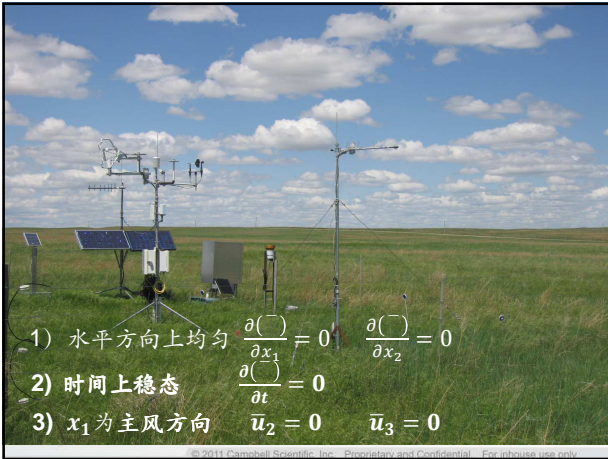
$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{\partial p_1}{\rho_0 \partial x_i} + \frac{\mu}{\rho_0} \frac{\partial^2 u_i}{\partial x_j \partial x_j} + \frac{T_1}{T_0} g \delta_{3i}$$

$$\frac{\partial (\bar{u}_i + u'_i)}{\partial t} + (\bar{u}_j - u'_j) \frac{\partial (\bar{u}_i + u'_i)}{\partial x_j} = -\frac{\partial (\bar{p}_1 + p'_1)}{\rho_0 \partial x_i} + \frac{\mu}{\rho_0} \frac{\partial^2 (\bar{u}_i + u'_i)}{\partial x_j \partial x_j} + \frac{\bar{T}_1 - \theta'}{T_0} g \delta_{3i}$$

$$\frac{\partial \bar{u}_i}{\partial t} + \bar{u}_j \frac{\partial \bar{u}_i}{\partial x_j} = -\frac{\partial \bar{p}_1}{\rho_0 \partial x_i} + \frac{1}{\rho_0} \frac{\partial}{\partial x_j} \left(\mu \frac{\partial \bar{u}_i}{\partial x_j} - \rho_0 \overline{u'_i u'_j} \right) + \frac{\bar{T}_1}{T_0} g \delta_{3i}$$



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1) 水平方向上均匀 $\frac{\partial(\quad)}{\partial x_1} = 0$ $\frac{\partial(\quad)}{\partial x_2} = 0$

2) 时间上稳态 $\frac{\partial(\quad)}{\partial t} = 0$

3) x_1 为主风方向 $\bar{u}_2 = 0$ $\bar{u}_3 = 0$

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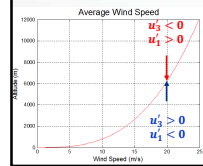
动量通量

$$\frac{\partial \bar{u}_1}{\partial t} + \bar{u}_j \frac{\partial \bar{u}_1}{\partial x_j} = -\frac{\partial \bar{p}_1}{\rho_0 \partial x_1} + \frac{1}{\rho_0} \frac{\partial}{\partial x_j} \left(\mu \frac{\partial \bar{u}_1}{\partial x_j} - \rho_0 \overline{u'_1 u'_j} \right) + \frac{\bar{T}_1}{T_0} g \delta_{31}$$

$$\bar{u}_3 \frac{\partial \bar{u}_1}{\partial x_3} = \frac{1}{\rho_0} \frac{\partial}{\partial x_3} \left(\mu \frac{\partial \bar{u}_1}{\partial x_3} - \rho_0 \overline{u'_1 u'_3} \right)$$

$$0 = \frac{1}{\rho_0} \frac{\partial}{\partial x_3} \left(\mu \frac{\partial \bar{u}_1}{\partial x_3} - \rho_0 \overline{u'_1 u'_3} \right)$$

$$\mu \frac{\partial \bar{u}_1}{\partial x_3} - \rho_0 \overline{u'_1 u'_3} = \text{常数}$$

$$-\rho_0 \overline{u'_1 u'_3} \approx \text{常数} > 0 \text{ (kg m/s)/(m}^2\text{s)}$$


动量通量

$$\tau = -\rho_0 \overline{u' w'}$$

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CO2通量

$$\frac{\partial \rho_{CO_2}}{\partial t} + \bar{u}_j \frac{\partial \rho_{CO_2}}{\partial x_j} = D_{CO_2} \frac{\partial^2 \rho_{CO_2}}{\partial x_j \partial x_j}$$

$$\frac{\partial(\bar{\rho}_{CO_2} - \rho'_{CO_2})}{\partial t} + (\bar{u}_j + u'_j) \frac{\partial(\bar{\rho}_{CO_2} - \rho'_{CO_2})}{\partial x_j} = D_{CO_2} \frac{\partial^2(\bar{\rho}_{CO_2} - \rho'_{CO_2})}{\partial x_j \partial x_j}$$

$$\frac{\partial \bar{\rho}_{CO_2}}{\partial t} + \bar{u}_j \frac{\partial \bar{\rho}_{CO_2}}{\partial x_j} = -\frac{\partial}{\partial x_j} \left(-D_{CO_2} \frac{\partial \bar{\rho}_{CO_2}}{\partial x_j} + \overline{\rho'_{CO_2} u'_j} \right)$$

$$0 = -\frac{\partial}{\partial x_3} \left(-D_{CO_2} \frac{\partial \bar{\rho}_{CO_2}}{\partial x_3} + \overline{\rho'_{CO_2} u'_3} \right)$$

$$-D_{CO_2} \frac{\partial \bar{\rho}_{CO_2}}{\partial x_3} + \overline{\rho'_{CO_2} u'_3} = \text{常数 mg/(m}^2\text{s)}$$

CO2通量

$$F_c = \overline{\rho'_{CO_2} w'}$$

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动量通量

$$\tau = -\rho_0 \overline{u' w'}$$

感热通量

$$H = \rho_0 C_p \overline{T' w'}$$

潜热通量

$$LE = L \rho'_{H_2O} \overline{w'}$$

潜热通量

$$LE = L \frac{M_w \rho_d}{M_d} \overline{\chi_{H_2O} w'}$$

CO2通量

$$F_c = \overline{\rho'_{CO_2} w'}$$

CO2通量

$$F_c = \frac{\rho_d}{M_d} \overline{\chi_{CO_2} w'}$$

痕量气体通量

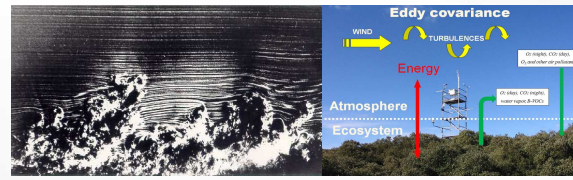
$$F_t = \overline{\rho'_t w'}$$

痕量气体通量

$$F_t = \frac{\rho_d}{M_d} \overline{\chi'_t w'}$$

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质能通量

$$F_x = C \overline{x' w'}$$


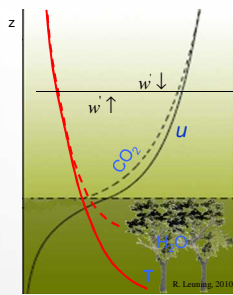
在近地面层，大气湍流传输质能，质能进入大气的通量是垂直涡动与质能标量的协方差，协方差为两个变量相关系数的分子，故这个质能通量被称为涡动相关通量。

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Example: 计算CO₂ 通量

$$F_C = \overline{w'\rho'_{CO_2}}$$



1 秒钟测定5次

<i>i</i>	ρ'_{CO_2} mg m ⁻³	w' m s ⁻¹	$\rho'_{CO_2}w'$ mg m ⁻² s ⁻¹
1	-20	0.2	-4
2	10	-0.1	-1
3	-30	0.1	-3
4	20	-0.2	-4
5	20	0	0
$\sum_{i=1}^5 \rho'_{CO_2}w'$			-12
$F_C = \overline{\rho'_{CO_2}w'} = \frac{1}{5} \sum_{i=1}^5 \rho'_{CO_2}w'$???



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本专题应回答的问题

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3. CO₂/H₂O/温度/风速垂直梯度 (结构)
4. 湍流传输CO₂/H₂O/热



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湍流的产生与耗散及其综合描述原理



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湍流的产生与耗散度量 (传统表达)

$$e = \frac{\rho}{2} (\overline{u'^2} + \overline{v'^2} + \overline{w'^2})$$

$$\frac{de}{dt} = 0 \quad \text{无湍流的产生与耗散}$$

$$\frac{de}{dt} > 0 \quad \text{产生湍流}$$

$$\frac{de}{dt} < 0 \quad \text{耗散湍流}$$



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湍流生散方程

$$\frac{De}{Dt} = -\rho \overline{(u'w')} \frac{\partial \bar{u}}{\partial z} + \rho \frac{g}{T} \overline{(T'w')} + \frac{\partial \overline{(p'w')}}{\partial z} - \frac{\rho}{2} \frac{\partial \overline{ew'}}{\partial z} - \rho \epsilon$$

↑ 动能变化 ↑ 下垫面摩擦 ↑ 气团沉浮 ↑ 压力运输 ↑ 湍流运输 ↑ 粘滞扩散

产生湍流: 垫面摩擦 气团上浮

耗散湍流: 气团下沉 粘滞扩散

运输湍流: 压力运输 湍流运输



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摩尼奥布科夫长度与大气边界层稳定度

$$\frac{De}{Dt} = -\rho \overline{(u'w')} \frac{\partial \bar{u}}{\partial z} + \rho \frac{g}{\bar{T}} \overline{(T'w')} + \frac{\partial \overline{(p'w')}}{\partial z} - \frac{\rho}{2} \frac{\partial \overline{ew'}}{\partial z} - \rho \epsilon$$

$$u_* = [\overline{(u'w')^2}]^{1/4}$$

近地面层
大气稳定度

摩尼奥布科夫长度
Monin-Obukhov length

$$\frac{z}{L} = -\frac{(g/\bar{T})\overline{T'w'}}{u_*^3/kz}$$

$$L = -\frac{u_*^3/k}{(g/\bar{T})\overline{(T'w')_0}}$$

无量纲

描述整个大气近地面



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大气边界层稳定度的应用

$$\frac{z}{L} = -\frac{(g/\bar{T})\overline{T'w'}}{u_*^3/kz}$$

According to Monin-Obukhov hypothesis, various atmospheric parameters and statistics such as gradients, variances, and covariance; when normalized by appropriate of the scaling velocity u_* and scaling temperature T_* ; **become universal functions of z/L**

[p15, Kaimal & Finnigan (1994).

$$u_* = \left[-\overline{(u'w')_0} \right]^{1/2} \quad T_* = \frac{-\overline{(w'T')_0}}{u_*}$$



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风速和温度梯度为大气边界层稳定度的函数

p14, Kaimal & Finnigan (1994)

$$\frac{\partial u}{\partial z} = \frac{u_*}{kz} \begin{cases} \left(1 + 16 \left|\frac{z}{L}\right|\right)^{1/4} & -2 \leq \frac{z}{L} \leq 0 \\ \left(1 + 5 \frac{z}{L}\right) & 0 \leq \frac{z}{L} \leq 1 \end{cases}$$

$$\frac{\partial \theta}{\partial z} = \frac{T_*}{kz} \begin{cases} \left(1 + 16 \left|\frac{z}{L}\right|\right)^{1/2} & -2 \leq \frac{z}{L} \leq 0 \\ \left(1 + 5 \frac{z}{L}\right) & 0 \leq \frac{z}{L} \leq 1 \end{cases}$$



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风速和温度波动为大气边界层稳定度的函数

p14, Kaimal & Finnigan (1994)

$$\sigma_w = u_* \begin{cases} 1.25 \left(1 + 3 \left|\frac{z}{L}\right|\right)^{1/3} & -2 \leq \frac{z}{L} \leq 0 \\ 1.25 \left(1 + 0.2 \frac{z}{L}\right) & 0 \leq \frac{z}{L} \leq 1 \end{cases}$$

$$\sigma_\theta = T_* \begin{cases} 2 \left(1 + 9.5 \left|\frac{z}{L}\right|\right)^{-1/3} & -2 \leq \frac{z}{L} \leq 0 \\ 2 \left(1 + 0.5 \frac{z}{L}\right)^{-1} & 0 \leq \frac{z}{L} \leq 1 \end{cases}$$



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湍流动能耗散系数为大气边界层稳定度的函数

p14, Kaimal & Finnigan (1994)

$$\epsilon = \frac{u_*^3}{kz} \begin{cases} \left(1 + 0.5 \left|\frac{z}{L}\right|\right)^{3/2} & -2 \leq \frac{z}{L} \leq 0 \\ \left(1 + 5 \frac{z}{L}\right) & 0 \leq \frac{z}{L} \leq 1 \end{cases}$$



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本专题应回答的问题

1. 边界层及其高度
2. 湍流的产生和耗散与其随机运动
3. CO₂/H₂O/温度/风速垂直梯度 (结构)
4. 湍流传输CO₂/H₂O/热



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Table 1. Velocity scales (friction velocity, u_* , and convective velocity scale, w_*), Obukhov length (L), and planetary boundary layer height (h) characterising the stability regimes of LPDM-B simulations at measurement height z_m and with roughness length z_0 . Cases with measurement height within the roughness sublayer were disregarded (see text for details).

Scenario	u_* [m s^{-1}]	w_* [m s^{-1}]	L [m]	h [m]
1 convective	0.2	1.4	-15	2000
2 convective	0.2	1.0	-30	1500
3 convective	0.3	0.5	-650	1200
4 neutral	0.5	0.0	∞	1000
5 stable	0.4	-	1000	800
6 stable	0.4	-	560	500
7 stable	0.3	-	130	250
8 stable	0.3	-	84	200

Receptor heights at $z_m/h = [0.005, 0.01, 0.075, 0.25, 0.50]$
 Roughness lengths $z_0 = [0.01, 0.1, 0.3, 1.0, 3.0]$ m

Kijun et al (2015)

回答问题完毕

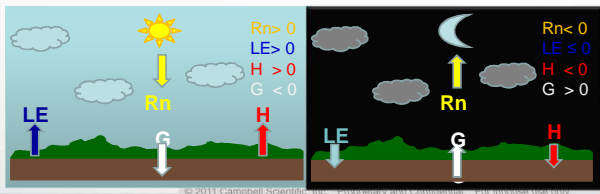
1. 边界层及其高度
2. 湍流的产生和耗散与其随机运动
3. $\text{CO}_2/\text{H}_2\text{O}/\text{温度}/\text{风速}$ 垂直梯度 (结构)
4. 湍流传输 $\text{CO}_2/\text{H}_2\text{O}/\text{热}$

近地面层大气稳定度

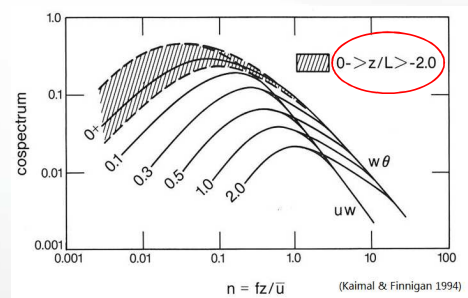
$$\frac{z}{L} = - \frac{(g_0 / \bar{T}) \overline{w'T'}}{u_*^3 / kz}$$

$\frac{z}{L} < 0$ 近地面层非稳定

$\frac{z}{L} > 0$ 近地面层稳定



垂直风速与水平风速或温度 在大气边界层不同稳定性下的协湍流谱



主要参考文献

- Kaimal, J.C. and J.J. Finnigan. 1994. Atmospheric Boundary Layer Flows: Their Structure and Measurements. Oxford University Press, New York, NY. 289 pp.
- Lumley, J.L. and Panofsky. 1964. The structure of Atmospheric Turbulence. John Wiley and Sons, Inc. 239 pp.
- Wallace, J.M. and P.V. Hobbs. 2006. Atmospheric Science: An introductory Survey.
- Schlichting, H. 1960. Boundary Layer Theory. 4th ed. McGraw-Hill Co., Inc. 647 pp.
- Stull, R.B. 1988. An introduction to Boundary-Layer Meteorology. Kluwer Academy Publishers, Boston. 666 pp.

Questions ?



谢谢!



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